## In the Claims:

This listing of claims will replace all prior versions, and listings, of claims in the application.

- 1. (Cancelled)
- 2. (Currently amended) Method according to claim [[ $\frac{1}{2}$ ]  $\underline{8}$ , wherein the preset offset value for the balance flow ( $f_{bal}$ ) is greater than zero, whereby the positive sign indicates a flow from the working path in the direction of the excess path.
- 3. (Currently amended) Method according to claim [[4]]  $\underline{8}$ , wherein the dependency of the sensor signal (S<sub>bal</sub>) of the flow sensor (108) on at least one property of the fluid is corrected in such fashion during the adjustment of the balance flow (f<sub>bal</sub>) that the preset offset value for the balance flow (f<sub>bal</sub>) results.
- 4. (Previously presented) Method according to claim 3, wherein for the correcting purposes a correction parameter is linked to the sensor signal (S<sub>bal</sub>).
- 5. (Previously presented) Method according to claim 3, wherein the values for the correction factor are stored in a lookup table, or the functional dependency of the correction factor from at least one property of the fluid is stored.
- 6. (Currently amended) Method according to claim [[4]]  $\underline{8}$ , wherein the balance flow (f<sub>bal</sub>) in order to achieve a temporary reduction of the external work flow (f<sub>ew</sub>) further down the working path is adjusted to a preset value that is high in comparison to the offset value.
  - 7. (Canceled)
- 8. (Currently amended) [[Method according to claim 7, ]] Method to supply a defined fluid flow, especially for liquid chromatography,

- a) in which a total flow  $(f_0)$  is split into an internal excess flow  $(f_{ie})$  in an excess branch and an internal work flow  $(f_{iw})$  in a working branch.
- b) wherein the split ratio between the internal work flow  $(f_{iw})$  and the internal excess flow  $(f_{ie})$  is determined by the reverse ratio of a fluidic resistor (7) in the working branch and fluidic resistor (9) in the excess branch, and
- c) where the excess branch and the working branch are interconnected at the outputs of the two fluidic resistors (7, 9) via a cross-branch,
- d) in which the balance flow  $(f_{bal})$  occurring between the outputs of the fluidic resistors (7, 9) is measured with a flow sensor (108),
- e) where further down the working branch an external work flow ( $f_{ew}$ ) can be supplied to an operating device downstream of the device (100),
- f) after which further down the excess branch an adjustable resistance device (11) is installed,
- g) where by control of the resistance value of the adjustable fluidic resistance device (110) the balance flow ( $f_{bal}$ ) is regulated in such manner that the balance flow ( $f_{bal}$ ) is in the temporal median, generally equal to zero or equal to a preset offset value, whose value is small in comparison to the internal work flow ( $f_{iw}$ ),

wherein the resistance value if the adjustable fluidic resistance device for the determination of the internal work flow ( $f_{iw}$ ) and/or external work flow ( $f_{ew}$ ) further down the working path is temporarily set in such manner that a balance flow ( $f_{bal}$ ) of unequal to zero results, and the internal work flow ( $f_{iw}$ ) expected in normal operating mode and/or the external work flow ( $f_{ew}$ ) is determined from the signal ( $f_{vai}$ ) of the flow sensor (108),

wherein the adjustable fluidic resistance device (110) is shorted for measuring the internal work flow ( $f_{iw}$ ) in the cross-branch and/or adjusted to a value equal to zero, whereby the cross-branch preferably exhibits a fluidic resistance of equal to or near zero.

## 9-12. (Canceled)

13. (Currently amended) Method according to claim [[4]] 8, wherein the total fluidic resistance value of the changeable fluidic resistance device (110) is composed of the resistance

value of an adjustable, preferably electrically controlled fluidic resistance element (122) and a non-adjustable fluidic resistance element (120), wherein the fluidic resistance value is dependent on the viscosity of the solvent being used.

- 14. (Currently amended) Method according to claim [[4]] 8, wherein the operating device is a chromatography column.
- 15. (Currently amended) [[Method according to claim 3,]] Method to supply a defined fluid flow, especially for liquid chromatography,
- a) in which a total flow  $(f_0)$  is split into an internal excess flow  $(f_{ie})$  in an excess branch and an internal work flow  $(f_{iw})$  in a working branch,
- b) wherein the split ratio between the internal work flow  $(f_{iw})$  and the internal excess flow  $(f_{ie})$  is determined by the reverse ratio of a fluidic resistor (7) in the working branch and fluidic resistor (9) in the excess branch, and
- c) where the excess branch and the working branch are interconnected at the outputs of the two fluidic resistors (7, 9) via a cross-branch,
- d) in which the balance flow  $(f_{bal})$  occurring between the outputs of the fluidic resistors (7, 9) is measured with a flow sensor (108),
- e) where further down the working branch an external work flow ( $f_{ew}$ ) can be supplied to an operating device downstream of the device (100),
- <u>f)</u> after which further down the excess branch an adjustable resistance device (11) is installed,
- g) where by control of the resistance value of the adjustable fluidic resistance device (110) the balance flow ( $f_{bal}$ ) is regulated in such manner that the balance flow ( $f_{bal}$ ) is in the temporal median, generally equal to zero or equal to a preset offset value, whose value is small in comparison to the internal work flow ( $f_{iw}$ ),

wherein the dependency of the sensor signal ( $S_{bal}$ ) of the flow sensor (108) on at least one property of the fluid is corrected in such fashion during the adjustment of the balance flow ( $f_{bal}$ ) that the preset offset value for the balance flow ( $f_{bal}$ ) results,

wherein the at least one property of the fluid is the thermal conductivity or thermal capacity of the fluid.

- 16. (Previously presented) Method according to claim 4, wherein a correction factor is multiplied with the sensor signal  $(S_{bal})$ .
  - 17. (Canceled)
- 18. (Previously presented) Method according to claim 13, wherein the fluidic resistance value is that of the non-adjustable fluidic resistance element (120).